



# Landscape evolution models using the stream power incision model show unrealistic behavior when $m/n$ equals 0.5

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**Abstract.** Landscape evolution models often utilize the stream power incision model to simulate river incision:  $E=KA^mS^n$ , where  $E$  = vertical incision rate,  $K$  = erodibility constant,  $A$  = upstream drainage area,  $S$  = channel gradient, and  $m$  and  $n$  are exponents. This simple but useful law has been employed with an imposed rock uplift rate to gain insight into steady-state  
10 landscapes. The most common choice of exponents satisfies  $m/n = 0.5$ ; indeed, this ratio has been deemed to yield the “optimal channel network.” Yet all models have limitations. Here, we show that when hillslope diffusion (which operates only at small scales) is neglected, the choice  $m/n = 0.5$  yields a curiously unrealistic result: the predicted landscape is invariant to horizontal stretching. That is, the steady-state landscape for a  $1 \text{ m}^2$  horizontal domain can be stretched so that it is identical to the corresponding landscape for a  $100 \text{ km}^2$  domain.

## 15 1 Introduction

The stream power incision model (SPIM) (e.g., Howard, 1994; Howard et al., 1994) is a commonly-used physically-based model for bedrock incision. The incision rate,  $E$ , can be written as

$$E = KA^mS^n \tag{1}$$

where  $K$  = erodibility coefficient,  $A$  = upslope drainage area,  $S$  = downstream slope, and  $m$  and  $n$  are exponents. This simple  
20 model is thoroughly reviewed in Whipple and Tucker (1999) and Lague (2014), where they hypothesize that  $m/n$  is between 0.35 and 0.60. This range is consistent with results inferred from field work and map studies (Flint, 1974; Howard and Kerby, 1983; Tarboton et al., 1989; Willgoose et al., 1990; Tarboton et al., 1991; Willgoose, 1994; Moglen and Bras, 1995; Snyder et al., 2000; Banavar et al., 2001). Furthermore, researchers specifically suggest that the ratio,  $m/n \sim 0.5$  (Snyder et al., 2000; Banavar et al., 2001). The choice of this ratio is paramount in numerical Landscape Evolution Models (LEMs) that utilize  
25 SPIM, such as the channel-hillslope integrated landscape development model, *CHILD* (Tucker et al., 2001). The ratio,  $m/n$ , is also used to describe the relationship between slope and drainage area in describing stream long profiles (Flint, 1974). All models using SPIM, including studies on drainage reorganization and stability (Willett et al., 2014), tectonic histories of landscapes (Goren et al., 2014b; Fox et al., 2014), and persistent drainage migration (Pelletier, 2004), involve specification of this ratio. In addition, the specific values of  $m$  and  $n$  are important (Tucker and Whipple, 2002). Here, however, we focus on



the ratio itself. In their research on optimal channel networks, Rodriguez-Iturbe and Rinaldo (2001) hypothesize that a landscape's drainage network organizes itself into an optimal state which minimizes the rate of energy dissipation. Their definition of optimality requires that  $m/n = 0.5$ . Here, however, we show a somewhat unexpected result: when  $m/n = 0.5$ , SPIM-based LEMs exhibit elevation solutions that are invariant to shape-preserving stretching of horizontal domain. That is, except for the finest scales at which hillslope diffusion becomes important, the model predicts the same solution for a landscape with a total basin area of  $1 \text{ m}^2$  and one with a total basin area of  $100 \text{ km}^2$  under the constraint of identical horizontal basin shape (e.g. square). The validity of SPIM at the meter scale should not be expected, but the extremity of this result underscores a heretofore unrecognized unrealistic aspect of SPIM.

10 In this paper, we perform a scaling analysis of SPIM. First, we use a 1D model to analytically derive steady-state river profiles, to illustrate the problem of scale invariance, and to delineate conditions for which elevation singularities occur at the ridge. Then, using a 2D numerical model, we demonstrate the effects of horizontal scale on the steady-state relief of landscapes and infer the conditions for which elevation singularities occur at ridges.

## 2 Motivation

15 SPIM is a simple model that has been used to gain considerable insight into landscape evolution. Previous studies using SPIM have shown how landscapes respond to tectonic and climate forcing (e.g., Howard, 1994; Howard et al., 1994). Yet like most simple models, SPIM is in some sense an oversimplification. Here we demonstrate this by showing that it satisfies a curiously unrealistic scale invariance relation. By demonstrating this limitation, we hope to motivate the formulation of models that overcomes it.

20 The fundamental limitation on SPIM becomes apparent when the ratio,  $m/n = 0.5$ . Under this condition, a SPIM will predict the same steady-state relief for a  $1 \text{ m}^2$  domain as a  $100 \text{ km}^2$  domain of the same horizontal shape, as illustrated below. LEMs utilizing SPIM often sidestep this problem with the use of a "hillslope diffusion" coefficient (Passalacqua et al., 2006), a useful but rather poorly-constrained parameter that lumps together a wide range of processes (Fernandes and Dietrich, 1997).

25 Alternatively, the problem can be sidestepped with an externally specified "hillslope critical length" (Goren et al., 2014a) that essentially specifies the location of channel heads. For example, the model simulations of Willett et al. (2014) employ the specific value of 500 m for hillslope critical length in their characterization of tendencies for drainage divide migration. The prediction of the hillslope diffusion coefficient and the location of channels are outstanding problems in the field of geomorphology (Montgomery and Dietrich, 1988). The intrinsic nature of the SPIM model, however, is such that scale invariance persists for the case  $m/n = 0.5$  at scales larger than a characteristic hillslope length scale, whether it be externally specified or computed from a diffusion coefficient.

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The existence of scale invariance exemplifies an unrealistic aspect of SPIM, which we believe to be associated with its omission of natural processes, such as abrasion due to sediment transport. Gilbert (1877) theorized two roles that sediment moving as bedload could play in bedrock incision, the first as an abrasive agent that incises the bed via collisions and the second as a protector that inhibits collisions of bedload on the bed. These observations have been implemented quantitatively by many modelers (e.g., Sklar and Dietrich, 2001, Sklar and Dietrich, 2004; Sklar and Dietrich, 2006; Lamb et al., 2008; Zhang et al., 2015), some of whom have implemented them in LEMs (e.g. Gasparini et al., 2006, Gasparini et al., 2007). Here we shed light on an unrealistic behavior of SPIM with the goal of motivating the landscape evolution community to develop more advanced treatments that better capture the underlying physics. A further goal is to emphasize the importance of scaling and non-dimensionalization in characterizing LEMs.

### 10 3 1D model: scale invariance and singularities

A LEM can be implemented using the following equation of mass conservation for rock/regolith subject to uplift and denudation:

$$\partial\eta/\partial t = v - E - D\nabla^2\eta \quad (2)$$

where  $\eta$  = local landscape elevation,  $t$  = time,  $v$  = rock uplift rate and  $D$  = hillslope diffusion coefficient. The term,  $D\nabla^2\eta$ , accounts for hillslope diffusion (Somfai and Sander, 1997; Banavar et al., 2001). The effect of diffusion is commonly neglected at coarse-grained resolution (Somfai and Sander, 1997; Banavar et al., 2001; Passalacqua et al., 2006), at which any resolved channels can be taken to be fluvially-dominated bedrock channels (Montgomery and Foufoula-Georgiou, 1993). In our analysis, we use Eq. (1) to specify the incision term in Eq. (2). It should be noted that SPIM refers to the incision in the direction normal to the bed, implying that there are both horizontal and vertical components of incision. In much of the literature using SPIM, however, the horizontal component is neglected in accordance with the original formulation of Howard and Kerby (1983), and incision is assumed to be purely vertical downward: Here we preserve this simplification in order to better understand the overall behavior of SPIM.

Equation (2) characterizes landscape evolution in 2D; i.e. elevation  $\eta = \eta(x,y)$ , where  $x$  and  $y$  are horizontal coordinates. It is useful for some purposes, however, to simplify Eq. (2) into a 1D form. Neglecting hillslope diffusion, the 1D conservation equation is

$$\partial\eta/\partial t = v - KA^m(-\partial\eta/\partial l)^n \quad (3)$$

where  $l$  = horizontal stream distance from the ridge, at which  $l = 0$ . It should be noted that the negative sign appears front of the term  $\partial\eta/\partial l$  because  $\partial\eta/\partial l$  is negative in the downstream direction, so that streambed slope,  $S = -\partial\eta/\partial l$ . In SPIM, slope  $S$  is assumed to be positive. In order to solve Eq. (3), a relationship between  $A$  and  $l$  must be established. Here we assume a generalized form of Hack's Law (Hack, 1957);

$$A = Cl^h \quad (4)$$



where  $C$  and  $h$  are positive values. Hack's Law assumes that upslope area increases with  $l^h$ . From empirical data, Hack found the exponent,  $h$ , to be  $\sim 1.67$  (Hack, 1957).

Previous researchers have presented 1D analytical solutions for elevation profiles (Chase, 1992; Beaumont et al., 1992, 5 Anderson, 1994; Kooi and Beaumont, 1994; Tucker and Slingerland, 1994; Kooi and Beaumont, 1996; Densmore et al., 1998; Willett, 1999; Whipple and Tucker, 1999; Willett, 2010). In their solutions, the effect of the horizontal scale, which in the 1D model we define as the total length of the stream profile,  $L_{1D}$ , was neither shown nor discussed. Previous studies that use Eq. (4) (Whipple and Tucker, 1999; Willett, 2010) involve nondimensionalization of both the horizontal and vertical coordinates by the total horizontal length of the profile,  $L_{1D}$ . This step obscures the effect of the horizontal scale on the relief of the profile. 10 In our study, we nondimensionalize the vertical coordinate,  $\eta$ , by a combination of  $v$  and the acceleration of gravity,  $g$ . Our nondimensionalization of the coordinates is shown below.

$$\eta = v^2 g^{-1} \hat{\eta} \quad t = v g^{-1} \hat{t} \quad l = L_{1D} \hat{l} \quad (5)$$

Substituting Eq. (4) and Eq. (5) into Eq. (3) results in the following dimensionless conservation equation:

$$\partial \hat{\eta} / \partial \hat{t} = 1 - P_{1D}^{-n} \hat{l}^{hm} (-\partial \hat{\eta} / \partial \hat{l})^n \quad (6)$$

15 where the dimensionless number  $P_{1D}$ , termed the 1D Pillsbury number herein for convenience, is given by the relation

$$P_{1D} = K^{-1/n} C^{-m/n} L_{1D}^{1-hm/n} v^{1/n-2} g \quad (7)$$

At steady-state, Eq. (6) becomes

$$P_{1D} = \hat{l}^{hm/n} (-\partial \hat{\eta} / \partial \hat{l}) \quad (8)$$

From this equation, we see as we approach the ridge, i.e.  $\hat{l} \rightarrow 0$ , the slope term  $(-\partial \hat{\eta} / \partial \hat{l})$  always approaches infinity for 20 positive values of  $h$ ,  $m$ , and  $n$ .

The value of the 1D Pillsbury number  $P_{1D}$  increases with stream profile length,  $L_{1D}$ , when  $hm/n < 1$ , is invariant to changes in  $L_{1D}$  when  $hm/n = 1$ , and decreases with  $L_{1D}$  when  $hm/n > 1$ . This can be further illustrated by integrating Eq. (8). To solve this first order differential equation, we need to specify a single boundary condition, shown below.

$$25 \quad \hat{\eta}|_{\hat{l}=1} = 0 \quad (9)$$

This boundary condition sets the location and elevation of the outlet, where flow is allowed to exit the system. Integrating Eq. (8) yields

$$\hat{\eta} = \begin{cases} -P_{1D} \ln(\hat{l}) & \text{if } hm = n \\ (1 - hm/n)^{-1} P_{1D} (1 - \hat{l}^{1-hm/n}) & \text{if } hm \neq n \end{cases} \quad (10)$$

The steady-state profiles defined by Eq. (10) are shown in Fig. 1. Inspecting Eq. (10), we see that elevation is infinite at the 30 ridge ( $l = 0$ ) when  $hm/n \geq 1$ , and elevation is finite when  $hm/n < 1$ . In addition, when  $hm/n = 1$ ,  $P_{1D}$ , shown in Eq. (7), is no longer dependent on the horizontal scale,  $L_{1D}$ , and  $\hat{\eta}$  is independent of the scale of the basin. Using the empirical value from



Hack's original work (1957), i.e.  $h = 1.67$ , the ratio,  $m/n$ , must take the value 0.6 for scale invariance. This ratio is within the range reported in the literature (Whipple and Tucker, 1999).

#### 4 2D model: scale invariance

In 2D, the conservation equation using SPIM and neglecting hillslope diffusion can be written as

$$5 \quad \partial\eta/\partial t = v - KA^m[(\partial\eta/\partial x)^2 + (\partial\eta/\partial y)^2]^{n/2} \quad (11)$$

To understand the behavior of Eq. (11) in response to scale, we need to use a dimensionless formulation in a fashion similar to the previous 1D analysis. Here,  $L_{2D}$  denotes the horizontal length of the entire domain, which is taken to be square for convenience. For the 2D analysis, our nondimensionalization is

$$\eta = v^2 g^{-1} \hat{\eta} \quad t = vg^{-1} \hat{t} \quad A = L_{2D}^2 \hat{A} \quad x = L_{2D} \hat{x} \quad y = L_{2D} \hat{y} \quad (12)$$

10 The form of Eq. (11) in which  $x$ ,  $y$ , and  $A$  have been made dimensionless using the definitions shown in Eq. (12) is

$$\partial\hat{\eta}/\partial\hat{t} = 1 - P_{2D}^{-n} \hat{A}^m [(\partial\hat{\eta}/\partial\hat{x})^2 + (\partial\hat{\eta}/\partial\hat{y})^2]^{n/2} \quad (13)$$

where the dimensionless number  $P_{2D}$ , termed the 2D Pillsbury number is given as

$$P_{2D} = K^{-1/n} L_{2D}^{1-2m/n} v^{1/n-2} g \quad (14)$$

At steady-state, Eq. (13) becomes

$$15 \quad P_{2D} = \hat{A}^{m/n} [(\partial\hat{\eta}/\partial\hat{x})^2 + (\partial\hat{\eta}/\partial\hat{y})^2]^{1/2} \quad (15)$$

The form of the parameter  $P_{2D}$  specified by Eq. (14) is similar to the 1D form, Eq. (7), but different due to the different dimensionality. The parameter,  $P_{2D}$ , scales with the relief of the landscape; as it increases, the slope term on the RHS of Eq. (15) also increases. The value of  $P_{2D}$  increases with  $L_{2D}$  for  $m/n < 0.5$ , remains constant with  $L_{2D}$  for  $m/n = 0.5$ , and decreases with  $L_{2D}$  for  $m/n > 0.5$ . For the ratio,  $m/n = 0.5$ , the exponent above  $L_{2D}$  in Eq. (14) becomes zero, and the relief of the landscape becomes invariant to horizontal scale. When  $m/n = 0.5$ , the same steady-state solution to Eq. (15) prevails regardless of the value of  $L_{2D}$ .

Our 2D model was solved using the following boundary conditions:

$$\eta|_{y=0} = 0 \quad (16)$$

$$25 \quad \partial\eta/\partial y|_{y=L_{2D}} = 0 \quad (17)$$

$$\eta|_{x=0} = \eta|_{x=L_{2D}} \quad (18)$$

The bottom (outlet) side of the domain presented herein Fig. 2 is fixed at the base level  $\eta = 0$  m, corresponding to an open boundary where flow can exit the system while satisfying Eq. (16). The top side of the domain is designated as an impermeable boundary to flow, i.e. the drainage divide satisfies Eq. (17). Periodic boundary conditions satisfying Eq. (18) are applied at the

30 left and right boundaries. Flow, slope, and drainage area are determined using the D8 flow algorithm, where flow follows the



route of steepest descent (O’Callaghan and Mark, 1984). The initial condition is a gently-sloped plane oriented towards the outlet with small random perturbations.

For the results of Fig. 2, we used regular grids that contained  $100^2$  cells. The number of cells was constant, regardless of the value of  $L_{2D}$ . This is in contrast to making cell size constant, and increasing the number of cells with  $L_{2D}$ . We argue that the former shows the fundamental numerical behavior of SPIM, while the latter obscures the behavior due to the existence of slope and elevation singularities near the ridges in the landscape. The next sections show this singular behavior in the 2D numerical model.

Figure 2a shows steady-state solutions for  $m/n = 0.5$  and two values of  $L_{2D}$  using the same initial condition. At each corresponding grid cell between the two solutions, the slope,  $S$ , decreases as  $L_{2D}$  increases. However, the relief structures of each landscape are identical. By relief structure, we are describing the elevation value at each corresponding grid cell in the two steady-state solutions. This is confirmed by nondimensionalizing the horizontal scale of landscape without adjusting the vertical scale (Fig. 2b). Using the same numerical methods and the parameters from Fig. 2a, the results of a similar analysis using different ratios  $m/n = 0.4, 0.5$ , and  $0.6$  are shown in Fig. 2c.

In Fig. 2c, the case of scale invariance can be seen when  $m/n = 0.5$ . For  $m/n = 0.4$ , the relief of the entire landscape increases with increasing  $L_{2D}$ , and for  $m/n = 0.6$ , the relief decreases with increasing  $L_{2D}$ . When  $m/n \neq 0.5$ , the landscapes do not exhibit scale invariance. However, the overall planform drainage network structure shows resemblance across scales. That is, the location of the major streams and rivers in the numerical grid are similarly organized. It should be noted that the landscapes are not identical. When the landscapes are shown in dimensional space, as shown in Fig. 2a, the landscapes appear to be quite different. In the case of Fig. 2b, however, the smaller landscape can be stretched horizontally to be identical to the large one. The drainage network structure described above persists in each simulation due to the imprinting of the initial condition, which always consists of the same randomized perturbations.

## 5 2D model: quasi-theoretical analysis of singular behavior

Like the 1D model, Eq. (8), the 2D model, Eq. (15), has slope,  $S$ , approaching infinity as area,  $A$ , approaches zero at steady state. In contrast to the 1D model, however, general steady-state solutions for elevation in the 2D model, Eq. (15), cannot be determined analytically. However, the ratio,  $m/n$ , for which elevation singularities occur can be determined by analyzing the behavior of the 2D numerical model in close proximity to a ridge. Here, we first develop a quasi-theoretical treatment to study near-ridge behavior, which we then use to infer singular behavior in the numerical model. Converting the coordinate system from Cartesian to a system that follows the streamwise direction, we rewrite Eq. (11) as

$$\partial\eta/\partial t = v - KA^m(-\partial\eta/\partial s)^n \quad (19)$$



where  $s$  = distance along the path of steepest descent away from the ridge. From dimensional considerations,  $A$  [ $L^2$ ] must scale with  $s^2$  [ $L^2$ ] near the ridge ( $s = 0$ ), and therefore,

$$A = \beta s^2 \text{ as } s \rightarrow 0 \quad (20)$$

where  $\beta$  = scaling factor. For this analysis, our nondimensionalization is

$$5 \quad \eta = v^2 g^{-1} \hat{\eta} \quad t = v g^{-1} \hat{t} \quad s = L_R \hat{s} \quad (21)$$

where  $L_R$  = horizontal ridge scale. Near the ridge, Eq. (19) can be nondimensionalized into:

$$\partial \hat{\eta} / \partial \hat{t} = 1 - P_R^{-n} \hat{s}^{2m} (-\partial \hat{\eta} / \partial \hat{s})^n \quad (22)$$

where  $P_R$  is another dimensionless Pillsbury number, here denoted as

$$P_R = K^{-1/n} \beta^{-m/n} L_{1D}^{1-2m/n} v^{1/n-2} g \quad (23)$$

10 At steady-state ( $\partial \eta / \partial t = 0$ ), Eq. (22) becomes

$$P_R = \hat{s}^{2m/n} (-\partial \hat{\eta} / \partial \hat{s}) \quad (24)$$

From Eq. (24), we see that at the ridge ( $\hat{s} = 0$ ), there is a singularity in slope, i.e. the slope,  $(-\partial \hat{\eta} / \partial \hat{s})$ , goes to infinity.

Integration of Eq. (24) using the downstream boundary condition,  $\hat{\eta}|_{\hat{s}=1} = 0$ , allows for the delineation of the conditions for elevation singularities in the 2D model. The profile is given as

$$15 \quad \hat{\eta} = \begin{cases} -P_R \ln(\hat{s}) & \text{if } 2m = n \\ (1 - 2m/n)^{-1} P_R (1 - \hat{s}^{1-2m/n}) & \text{if } 2m \neq n \end{cases} \quad (25)$$

Instead of the elevation singularity occurring when  $hm/n \geq 1$  as seen in the 1D model, Eq. (10), this analysis for the 2D model shows an elevation singularity at the ridge when  $m/n \geq 0.5$ .

## 6 2D model: numerical analysis of singular behavior

Our quasi-theoretical analysis infers the conditions for singular behavior in the 2D model. If elevation singularities exist, the model will not satisfy grid-invariance, causing the relief between the ridge and outlet to increase indefinitely as grid size decreases. In contrast, in simulations where singularities do not exist, the relief between the ridge and outlet can be expected to converge as the grid size decreases. In both cases, understanding ridge behavior in the 2D model requires studying solution behavior as grid size approaches zero.

25 We do this by extracting river profiles from 13 landscape simulations of different scales for each value of  $m/n$ , i.e. 0.4, 0.5 and 0.6. The largest simulation is for  $L_{2D}^2 = 10^6$  km<sup>2</sup>; simulations were also performed at progressively one order-or-magnitude less in area down to  $L_{2D}^2 = 10^{-6}$  km<sup>2</sup>. The number of grid cells,  $M^2$ , is held constant at 25<sup>2</sup>. In each simulation, then, the closest distance to the ridge that can be resolved is one grid cell, given by

$$\Delta l_i = 10^{(7-i)/2} / 25 \text{ [km]} \quad i = 1, 2 \dots 13 \quad (26)$$

30 From each of the simulations, we construct two synthetic river profiles, one that intersects the highest point of the basin divide (high profile) and one that intersects the lowest point of the basin divide (low profile). The choice of these two elevations was





made so as to bracket the possible range of behavior; analogous results would be obtained from starting points along the basin divide at intermediate elevations. We use these synthetic profiles to characterize whether or not the numerical model is tending toward a singularity near ridges. We do this because the numerical model itself cannot directly capture singular behavior. We outline the details of the methodology for the high profile only, as the case of the low profile involves a transparent extension.

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The 13 simulations result in 13 elevation profiles  $\eta_i$ , where  $i = 1, 2, \dots, 13$  each extending from  $\Delta l_i$  (i.e. one grid point from the divide) to a downstream value  $l_{D_i}$  that is somewhat larger than the value  $10^{3-(i/2)}$  km (because the down-channel path of steepest descent does not follow a straight line.). We assemble a synthetic channel profile,  $\eta_S(l)$ , from these as follows. The first leg of  $\eta_S(l)$  is identical to  $\eta_1(l)$ , and extends from  $l = \Delta l_1$  to  $l_{D_1}$ . We extend the synthetic profile by translating the second profile upward until its elevation at its downstream point  $l_{D_2}$  matches with  $\eta_S(l_{D_2})$ , as shown in Fig. 3a. The profile,  $\eta_S(l)$ , now extends from  $\Delta l_2$  to  $l_{D_1}$ . As shown in Fig. 3a, we repeat this process until all 13 profiles have been used to assemble the synthetic profile, which now extends from  $\Delta l_{13}$  to  $l_{D_1}$ .

This procedure results in a high synthetic profile encompassing all thirteen profiles (circles) and in a low synthetic profile (crosses) (Fig. 3b). 1D analytical solutions, Eq. (10), are then fitted to the profiles of the 2D simulations using the 1D Pillsbury number,  $P_{1D}$ , as a fitting parameter. To account for the difference in dimensionality, the 1D steady-state profiles with  $hm/n = 0.8, 1.0, \text{ and } 1.2$  are fitted to the 2D data for  $m/n = 0.4, 0.5, \text{ and } 0.6$ , respectively. The scatter in the synthetic profile is due to the randomness in the pathway, as dictated by the initial conditions.

Figure 3b shows good fit between the 2D results and the corresponding 1D steady-state profiles. This allows us to make inferences concerning asymptotic behavior at a ridge. The analytical curves for elevation that best fit the 2D data for  $m/n < 0.5$  converge to finite values as  $l$  approaches 0 and infinity for  $m/n \geq 0.5$ . While these results do not constitute analytical proof of this asymptotic behavior, they provide strong evidence for it.

## 7 Discussion and conclusion

The 1D analytical solutions, Eq. (10) and Fig. 1, characterize the scale behavior of the SPIM, where there is scale invariance when  $hm/n = 1.0$ . In addition, the 2D numerical solution shown in Fig. 2 confirms the existence of the condition of scale invariance when  $m/n = 0.5$ . Models using SPIM with  $m/n = 0.5$  show the same relief structure regardless of the horizontal scale. Scale invariance of both the 1D and 2D models have not previously been demonstrated. This result calls into question the assertion that the ratio  $m/n = 0.5$ , which is the most commonly used ratio in landscape evolution models (e.g. Gasparini et al., 2006), represents an “optimal” value for a channel network (Rodriguez-Iturbe and Rinaldo, 2001). It also motivates further investigation as to why analysis of field data yields values of  $m/n \sim 0.5$  (Snyder et al., 2000; Banavar et al., 2001).





The numerical solutions of the 2D model allows inference that the 2D model cannot be grid-invariant for  $m/n \geq 0.5$ . In the absence of hillslope diffusion, ridges reach infinite elevation as grid size becomes vanishingly small. This result underlines the critical role of hillslope diffusion in obtaining meaningful results from the 2D model. Field estimates of hillslope diffusion have been obtained at the hillslope scale, but there are unanswered questions about their application in large-scale models  
5 (Fernandes and Dietrich, 1997). Our results suggest for the ratio,  $m/n < 0.5$ , there are steady-state grid-invariant solutions. However, the grid size below which grid-invariance is realized may be so small, e.g. sub-meter scale, that the validity of Eq. (1) is called into question. Issues with SPIM when used at large scale include the following. Studies commonly neglect the effect of hillslope diffusion when the scale of the grid is larger than the hillslope scale (Somfai and Sander, 1997; Banavar et al., 2001; Passalacqua et al., 2006). At coarse-grained scales, increasing the size of the numerical domain, while keeping the  
10 number of cells constant, will result in the behavior that shown in Fig. 2. That is, when  $m/n \geq 0.5$ , adding more cells to compensate for the size of the domain so that the grid size remains constant produces heavily biased (ever more singular) behavior near the ridges that does not represent the fundamental behavior of SPIM.

Our analysis illustrates that SPIM has two important limitations; a) unrealistic scale invariance when  $m/n$  takes the commonly-  
15 used value 0.5, so that a 1 m<sup>2</sup> basin has identical relief to a 100 km<sup>2</sup> basin, and b) singular behavior near the ridges for  $m/n \geq 0.5$  that makes maximum relief entirely and unrealistically dependent on grid size. SPIM has been used with much success to study the general behavior of landscapes (e.g., Howard, 1994; Howard et al., 1994). We believe, however, that the time has come to move on to more sophisticated models. While scientific questions remain that can be answered with the stream power incision model, there are many more questions that require a more advanced formulation (e.g., Crosby et al., 2007). The  
20 development of alternative, more physically-based models for incision (e.g. Sklar and Dietrich, 2004; Lague, 2014; Zhang et al., 2015) and their application to landscape evolution (e.g. Davy and Lague, 2009; Gasparini et al., 2006, 2007) offer exciting prospects for the future.

## 8 Notation

|             |   |
|-------------|---|
| <i>A</i>    | upslope drainage area [L <sup>2</sup> ]             |
| 25 <i>B</i> | profile width [L]                                   |
| <i>C</i>    | Hack's law constant [L <sup>2-h</sup> ]             |
| <i>D</i>    | hillslope diffusion coefficient [L <sup>2</sup> /T] |
| <i>E</i>    | local erosion rate [L/T]                            |
| <i>g</i>    | acceleration of gravity [L/T <sup>2</sup> ]         |
| 30 <i>h</i> | Hack's law exponent [-]                             |
| <i>K</i>    | erodibility coefficient [L <sup>(1-2m)</sup> /T]    |
| <i>i</i>    | index denoting the profile, 1,2...13 [-]            |



|    |              |  |
|----|--------------|--|
|    | $l$          | horizontal distance from the ridge in the 1D profile [L]                           |
|    | $\hat{l}$    | dimensionless horizontal distance from the ridge in the 1D profile, $l/L_{1D}$ [-] |
|    | $l_{Di}$     | total length of profile, $i$ [L]   |
|    | $l_i$        | horizontal distance from the ridge of profile, $i$ [L]                             |
| 5  | $L_{1D}$     | horizontal length scale, profile length [L]  |
|    | $L_{2D}$     | horizontal length scale, basin size [L]  |
|    | $L_R$        | horizontal length scale, ridge [L]   |
|    | $m$          | exponent above $A$ in SPIM [-]   |
|    | $M^2$        | number of numerical cells [cells <sup>2</sup> ]                                    |
| 10 | $n$          | exponent above $S$ in SPIM [-]   |
|    | $P_{1D}$     | Pillsbury number for the 1D analysis [-]   |
|    | $P_{2D}$     | Pillsbury number for the 2D analysis [-]   |
|    | $P_R$        | Pillsbury number for the 2D ridge analysis [-]                                     |
|    | $s$          | distance from the ridge [L]  |
| 15 | $\hat{s}$    | dimensionless distance from the ridge, $s/L_R$ [-]                                 |
|    | $S$          | stream gradient [-]  |
|    | $t$          | time [T]   |
|    | $\hat{t}$    | dimensionless time, $tg/v$ [-]   |
|    | $x$          | horizontal coordinate orthogonal to $y$ [L]  |
| 20 | $\hat{x}$    | dimensionless horizontal coordinate, $x/L_{2D}$ [-]                                |
|    | $y$          | horizontal coordinate orthogonal to $x$ [L]  |
|    | $\hat{y}$    | dimensionless horizontal coordinate, $y/L_{2D}$ [-]                                |
|    | $\beta$      | ridge scaling constant [-]   |
|    | $\Delta l_i$ | grid size for profile, $i$ [L]   |
| 25 | $\eta$       | elevation [L]  |
|    | $\hat{\eta}$ | dimensionless elevation, $\eta g/v^2$ [-]  |
|    | $\eta_i$     | elevation of profile, $i$ [L]  |
|    | $\eta_S$     | elevation of synthetic profile [L]   |
|    | $v$          | uplift rate [L/T]  |



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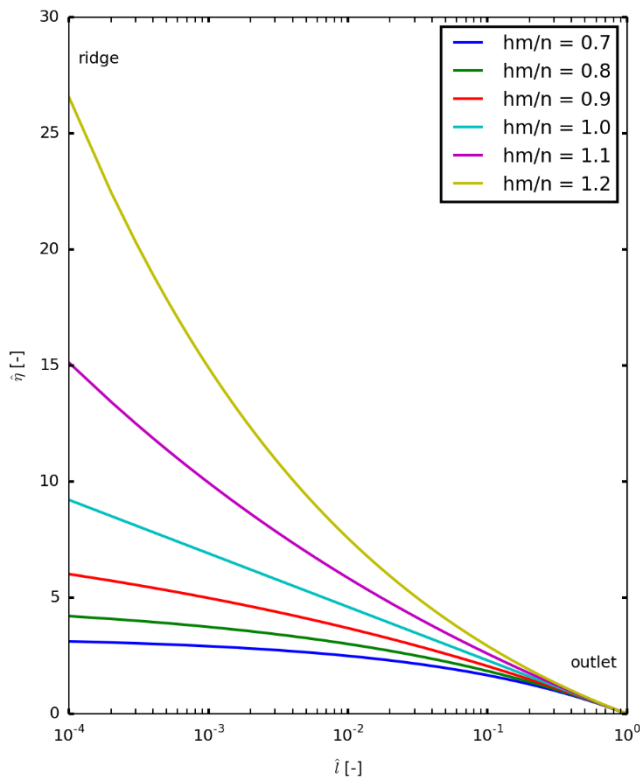
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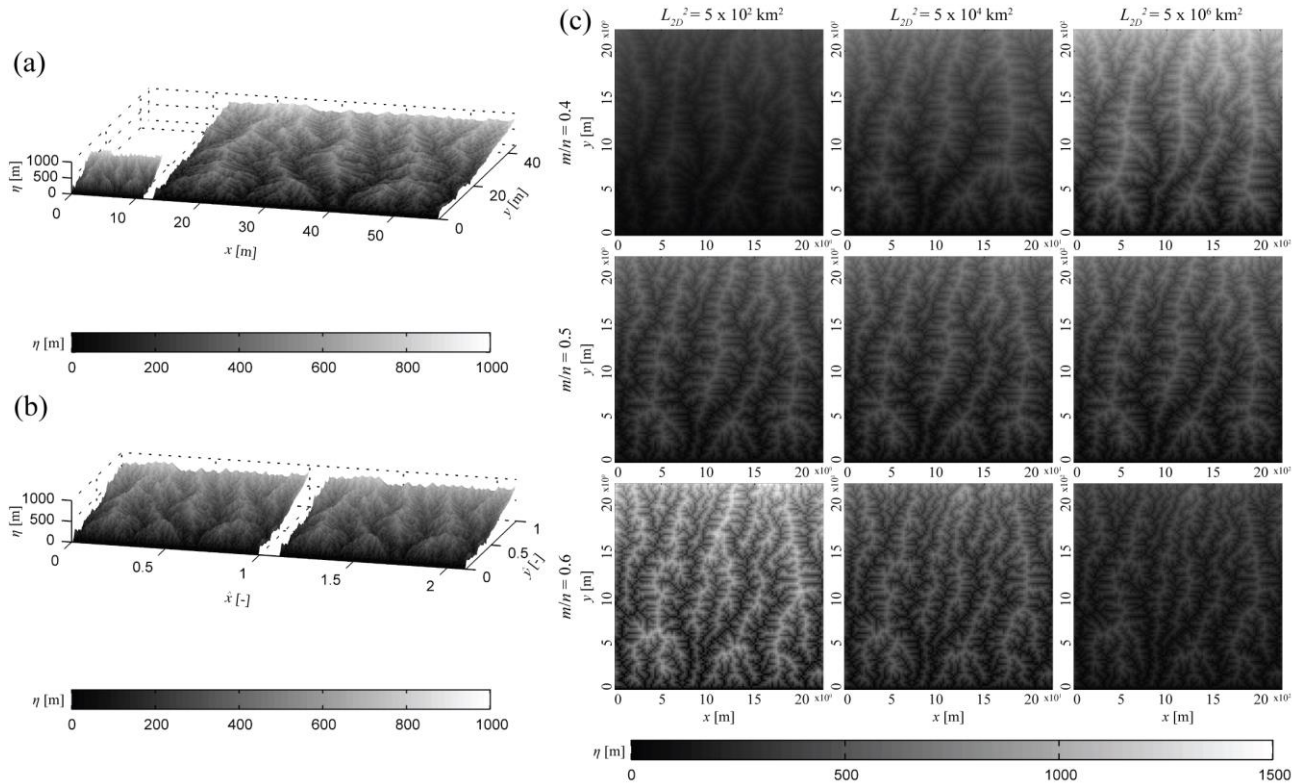
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15 **Figure 1:** 1D analytical dimensionless solutions for elevation profiles at steady-state equilibrium over a range of ratios  $hm/n$  (Hack's Law) = 0.7, 0.8, 0.9, 1.0, 1.1, and 1.2 and  $P_{1D} = 1.0$ .



5 **Figure 2:** (a) 2D numerical landscapes at steady-state using a ratio of  $m/n = 0.5$ ,  $n = 1.0$ ,  $v = 4 \text{ mm/yr}$ ,  $K = 2.83 \times 10^{-11} \text{ s}^{-1}$ ,  $M^2 = 1002$  cells, and  $L_{2D}^2 = 125 \text{ km}^2$  and  $2000 \text{ km}^2$ . For each case, the 2D Pillsbury number was the same,  $2.73 \times 10^{21}$ . (b) Results of (a) expressed in terms of dimensionless horizontal scale. Each basin is made dimensionless by its basin size,  $L_{2D}$ . (c) Nine 2D numerical simulations at dynamic equilibrium for three different values of  $L_{2D}$ , and three different values of  $m/n$ . The value of  $K$  has been chosen to be different for each value of  $m/n$  for clarity in the figures. From left to right, the  $L_{2D}^2 = 5 \times 10^2 \text{ km}^2$ ,  $5 \times 10^4 \text{ km}^2$ , and  $5 \times 10^6 \text{ km}^2$ . To make the relief of the landscapes comparable, the 2D Pillsbury number,  $P_{2D}$ , is set to  $2.73 \times 10^{21}$  for solutions of all  $m/n$  ratios with  $L_{2D}^2 = 5 \times 10^2 \text{ km}^2$ . To achieve this for  $v = 4 \text{ mm/yr}$ ,  $K = 2.10 \times 10^{-10} \text{ m}^{0.2}/\text{s}$ ,  $2.83 \times 10^{-11} \text{ s}^{-1}$ , and  $3.82 \times 10^{-12} \text{ m}^{-0.2}/\text{s}$  for  $m/n = 0.4, 0.5$ , and  $0.6$ , respectively.



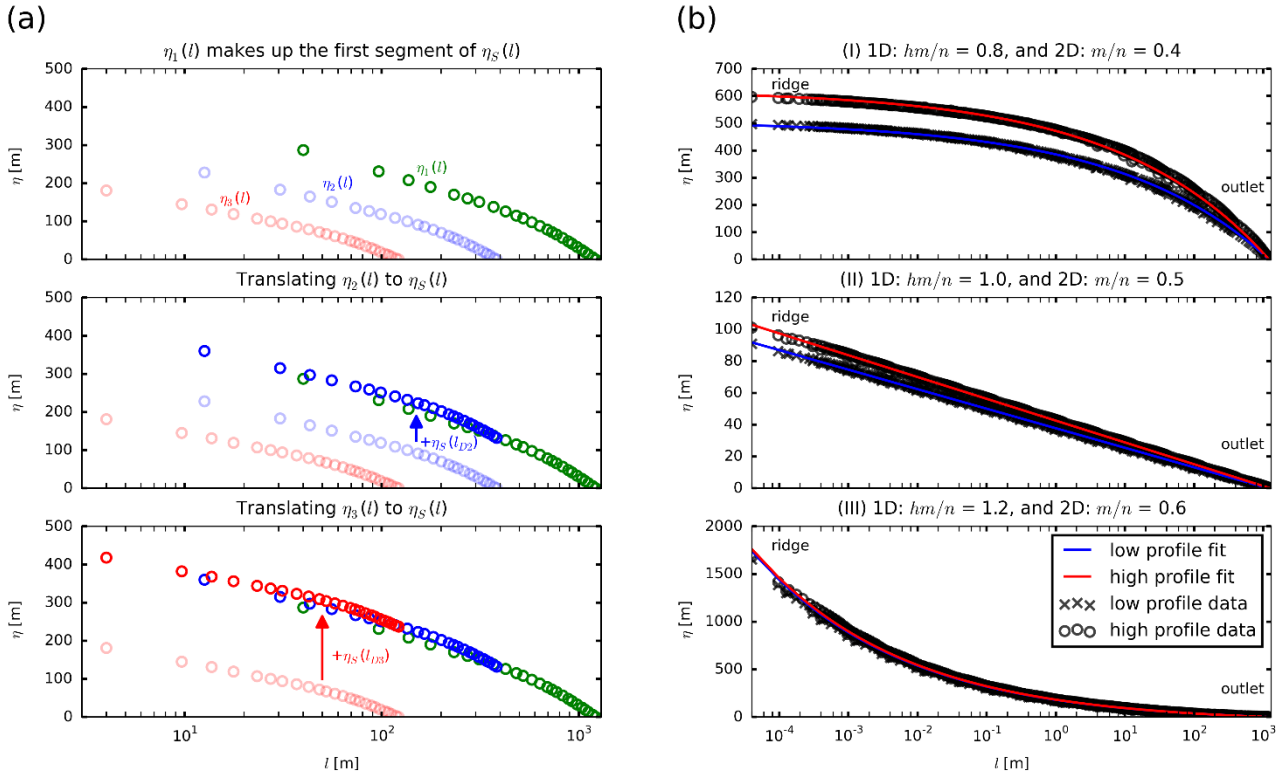


Figure 3: (a) Construction of the synthetic profile,  $\eta_S(l)$ . The opaque points represent the synthetic profile, and the transparent points represent the untranslated profiles. The green points represent the profile for  $i = 1$ , blue represent  $i = 2$ , and red represent  $i = 3$ . After  $\eta_{i3}(l)$  has been utilized in  $\eta_S(l)$ , the synthetic profile is complete. (b) 1D steady-state equilibrium analytical solutions fitted to 2D numerical results using  $P_{ID}$ . Each  $m/n$  ratio contains two profiles, one generated from a flow path from the highest point on the ridge corresponding to the basin divide (HP) and one from the lowest point on the basin divide (LP). The circles (HP) and crosses (LP) represent the 2D model data, and the red (HP) and blue (LP) line represent the 1D analytical model. For each  $m/n$  ratio,  $v = 3$  mm/yr,  $M^2 = 25^2$  cells,  $n = 1.0$ , and  $L_{2D}^2 = 10^{-6}$  km<sup>2</sup> to 10<sup>6</sup> km<sup>2</sup>. (I) Using  $K = 5.00 \times 10^{-12}$  m<sup>0.2</sup>/s,  $m/n = 0.4$  (2D), and  $hm/n = 0.8$  (1D),  $P_{ID} = 6.45 \times 10^{21}$  (LP) and  $P_{ID} = 7.89 \times 10^{21}$  (HP). (II) Using  $K = 2.83 \times 10^{-11}$  s<sup>-1</sup>,  $m/n = 0.5$  (2D), and  $hm/n = 1.0$  (1D),  $P_{ID} = 5.79 \times 10^{21}$  (LP) and  $P_{ID} = 6.47 \times 10^{21}$  (HP). (III) Using  $K = 3.82 \times 10^{-12}$  m<sup>0.2</sup>/s,  $m/n = 0.6$  (2D), and  $hm/n = 1.2$  (1D),  $P_{ID} = 2.13 \times 10^{23}$  (LP) and  $P_{ID} = 2.15 \times 10^{23}$  (HP).